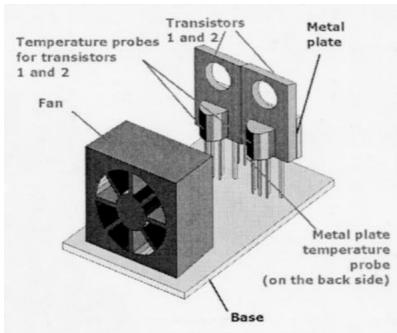


Automatic Control - Project 2016/2017
Control of a thermal process
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Consider the thermal process shown in the picture, and composed by two transistors attached to a metal plate, three temperature probes, two attached to the back side of each transistor and one attached to the plate, and a fan. The two transistors are used to heat the metal plate, whilst the fan can be powered in order to change the heat transfer coefficient between transistors and air or plate and air.

The nonlinear system describing the thermal process is



$$\begin{aligned} C_{t1}\dot{T}_1 &= P_{t1} - \gamma_{t1p}(T_1 - T_p) - \gamma_{t1a}(T_1 - T_a) \\ C_{t2}\dot{T}_2 &= P_{t2} - \gamma_{t2p}(T_2 - T_p) - \gamma_{t2a}(T_2 - T_a) \\ C_p\dot{T}_p &= \gamma_{t1p}(T_1 - T_p) + \gamma_{t2p}(T_2 - T_p) - \gamma_{pa}(T_p - T_a) \end{aligned}$$

where T_1, T_2, T_p, T_a , are the temperatures of the two transistors, the plate, and air, respectively; C_{t1}, C_{t2}, C_p , are the thermal capacities of the transistors and the plate, respectively; P_{t1}, P_{t2} , are the thermal powers generated by the two transistors; $\gamma_{t1p}, \gamma_{t2p}$, are the heat transfer coefficients from the transistors to the plate; $\gamma_{t1a}, \gamma_{t2a}$, and γ_{pa} , are the heat transfer coefficients from the transistors and the plate to the air.

The thermal powers, P_{t1}, P_{t2} , are related to the transistors' normalized commands, $Q_1, Q_2 \in [0, 100]$, by the following relations

$$P_{t1} = P_{max_{t1}} \left(k_{1_{t1}} \left(\frac{Q_1}{100} \right) + k_{2_{t1}} \left(\frac{Q_1}{100} \right)^2 \right) \quad P_{t2} = P_{max_{t2}} \left(k_{1_{t2}} \left(\frac{Q_2}{100} \right) + k_{2_{t2}} \left(\frac{Q_2}{100} \right)^2 \right)$$

where $k_{1_{t1}}, k_{2_{t1}}, k_{1_{t2}}$ and $k_{2_{t2}}$ are suitable constants, and $P_{max_{t1}}, P_{max_{t2}}$, are the maximum thermal powers generated by each transistor.

Finally, the heat transfer coefficients from the transistors to the air, γ_{t1a} and γ_{t2a} , and from the plate to the air, γ_{pa} , depend on the fan normalized command Q_f , varying from a minimum ($\Gamma_{t1a_0}, \Gamma_{t2a_0}, \Gamma_{pa_0}$) to a maximum ($\Gamma_{t1a_{100}}, \Gamma_{t2a_{100}}, \Gamma_{pa_{100}}$) as the fan command goes from 0 to 100, as described by the following relations

$$\gamma_{t1a} = \Gamma_{t1a_0} + (\Gamma_{t1a_{100}} - \Gamma_{t1a_0}) \frac{Q_f}{100} \quad \gamma_{t2a} = \Gamma_{t2a_0} + (\Gamma_{t2a_{100}} - \Gamma_{t2a_0}) \frac{Q_f}{100} \quad \gamma_{pa} = \Gamma_{pa_0} + (\Gamma_{pa_{100}} - \Gamma_{pa_0}) \frac{Q_f}{100}$$

Temperature measurements are affected by a zero mean Gaussian noise with amplitude $0.02^\circ C$.

Consider the following points:

1. Assuming $Q_f = 0$, and neglecting the nonlinearity in the thermal powers, P_{t1}, P_{t2} , derive the state-space linearized model and the transfer matrix, describing the thermal process.
2. Assuming again $Q_f = 0$ and $T_a = 20^\circ C$ and using the nonlinear simulator, identify a first order model describing the $Q_1 \rightarrow T_p$ relation (suggestion: consider a step response with $Q_1 = 50$ and $Q_2 = 0$). Verify the quality of the identified model considering different values of the input (i.e., $Q_1 = 10, 30, 70, \dots$), analysing and interpreting the results.
3. Compare the linear model identified in Step 2 with the linearized model computed in Step 1. Is the linear model identified in Step 2 accurate enough to design a linear controller?
4. Using the linear model identified in Step 2, design
 - a PI controller by cancellation, considering a limitation on the controller high frequency gain equal to $20 - 30 dB$,
 - a PI controller by cancellation, considering a limitation on the controller high frequency gain equal to $40 - 50 dB$,
 - a PID controller, not tuned by cancellation, considering a reasonable crossover frequency (with respect to the open-loop response time),

to regulate the plate temperature acting on transistor Q_1 .

5. Verify the performance of the regulators designed in Step 4 considering
 - (a) a reference plate temperature of $28^{\circ}C$, with $Q_f = 0$, $Q_2 = 0$ and $T_a = 20^{\circ}C$,
 - (b) a reference plate temperature of $28^{\circ}C$, with $Q_f = 50 \text{ step}(t - 500)$, $Q_2 = 40 \text{ step}(t - 1000)$ and $T_a = 20^{\circ}C$.

Analyse the results in terms of response time, disturbance rejection, control effort mitigation, etc.

6. Compute a digital realization of the controllers designed in Step 4, and simulate the digital control system assuming that the analogue to digital converter is characterised by 8 bit over a range of $0 - 50^{\circ}C$, and the digital to analogue converter is characterised by 12 bit over a range $0 - 100$. Perform the same simulations as in Step 5. If the suggested A/D and D/A converters cause an excessive performance degradation select a different number of bits.
7. Using Q_1 as control variable and assuming that only the plate temperature is measurable, design a pole placement controller in such a way that the closed-loop system response time is comparable to the response time obtained with the PID tuned in Step 4, and that zero-steady state tracking error of the plate temperature is ensured. Compare the performance achieved by the PID and the pole placement controller using the same simulation introduced in Step 5.

Rules

1. Each student carries out the project individually, solving as many points as possible (but not necessarily all the points).
2. System parameters depend on student's data and can be found in the attached table.
3. When the project is over, each student sends by email a short pdf report describing the project (including student's data), all the Simulink models and the .m files required to initialize the models (Simulink models and Matlab files should be compatible with Matlab/Simulink R2015b), to luca.bascetta@polimi.it.
4. Project report and all Matlab/Simulink files should be sent at least three working days before the date of the exam at which the student is enrolled.
5. Please do not enrol for the exam if you have not sent the project in due time.

858287	0,720	1,350	0,900	0,630	0,720	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
842310	0,879	1,647	1,098	0,769	0,879	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
863348	0,881	1,651	1,101	0,771	0,881	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
864796	0,881	1,651	1,101	0,771	0,881	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
853303	0,720	1,351	0,900	0,630	0,720	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
873062	0,881	1,653	1,102	0,771	0,881	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
852282	0,880	1,649	1,099	0,770	0,880	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
864004	0,881	1,651	1,101	0,771	0,881	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
864396	0,881	1,651	1,101	0,771	0,881	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
864357	0,719	1,349	0,899	0,629	0,719	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
853180	0,880	1,649	1,100	0,770	0,880	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
858283	0,720	1,350	0,900	0,630	0,720	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
876082	0,882	1,653	1,102	0,772	0,882	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
851545	0,721	1,351	0,901	0,630	0,721	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
850916	0,879	1,649	1,099	0,769	0,879	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150
851470	0,879	1,649	1,099	0,770	0,879	0,100	0,060	0,014	0,025	0,011	0,025	0,008	0,021	1,000	0,100	1,150	0,150