



3. Consider a single-track robot with front fixed wheel and rear steerable wheel. Assuming as configuration vector  $\mathbf{q} = [x \ y \ \theta \ \phi]^T$ , where  $(x \ y \ \theta)$  is the robot pose and  $\phi$  the steering angle, write the kinematic model of the robot without explicitly computing a base of  $\text{Null}(A^T(\mathbf{q}))$ .

## EXERCISE 2

1. What are the approaches that can be used to model the wheel-ground interaction? List them and explain the differences between them.

2. The longitudinal force in the brush or Fiala model is given by the following expression

$$F_x = \begin{cases} C_x \sigma_x \left( -1 + \frac{|\sigma_x|}{\sigma_{xsl}} - \frac{\sigma_x^2}{3\sigma_{xsl}^2} \right) & |\sigma_x| < \sigma_{xsl} \\ -\mu F_z \text{sign}(\sigma_x) & |\sigma_x| \geq \sigma_{xsl} \end{cases}$$

Explain the meaning of each symbol and of the wheel-ground interaction model equation.

3. Write the friction circle constraint and explain its meaning.

### ESERCIZIO 3

1. Define a feasible path planning problem and an optimal path planning problem, stressing the main differences between the two problems.

2. Describe the algorithm to construct the simplified probabilistic roadmap used by sPRM.

3. How the previous algorithm should be modified in order to transform it into its optimal version?

#### **ESERCIZIO 4**

1. Consider a robot described by the unicycle kinematic model, and a point  $P$  related to the unicycle wheel contact point  $(x, y)$  by the following relations

$$x_P = x + \varepsilon \cos \theta \quad y_P = y + \varepsilon \sin \theta$$

Show how a feedback control law that linearises the unicycle model can be derived.

2. Design a trajectory tracking controller based on the linearising law introduced in the previous step, and draw a block diagram of the entire control system, explaining how it can be tuned.

3. Explain why the control system designed in the previous step cannot control the robot heading.